REPORT OF SUBSURFACE EXPLORATION

PAVEMENT CORES – SHELBYVILLE ALONG RAMPART ROAD, MICHIGAN ROAD, AND MAUSOLEUM ROAD SHELBYVILLE, INDIANA PROJECT NUMBER: 23-1481-01G

PREPARED FOR:

THE CITY OF SHELBYVILLE 44 WEST WASHINGTON STREET SHELBYVILLE, INDIANA 46176

Patriot Engineering and Environmental, Inc. 6150 East 75th Street Indianapolis, Indiana 46250

November 8, 2023





November 8, 2023

Mr. John Kuntz, PE City of Shelbyville 44 West Washington Street, Shelbyville, Indiana 46176

Re: Report of Subsurface Exploration Pavement Cores – Shelbyville Along Rampart Road, Michigan Road, and Mausoleum Road Shelbyville, Indiana Patriot Project No.: 23-1481-01G

Dear John:

Attached is the report of our subsurface exploration for the above referenced project. This exploration was completed in general accordance with our Proposal No. P23-1759-01G dated September 20, 2023. This report includes graphic logs of nine (9) soil borings drilled at the proposed project site. Also included in the report are the results of laboratory tests performed on samples obtained from the site, and a pavement core summary.

The purpose of this exploration is to determine the general near surface and subsurface conditions within the project area of the existing roadways. This was achieved by pavement coring, drilling soil borings, and by conducting laboratory tests on soil samples taken from the borings. This report contains the results of our findings.

PROJECT INFORMATION

The proposed project is located along Rampart Road, Michigan Road, and Mausoleum Road and ends at Enterprise Drive in Shelbyville, Indiana. We understand that the new development proposed along Enterprise Drive will add about 500 new trucks per day along Rampart Road, Michigan Road, and Mausoleum Road. The Client would like to evaluate existing pavement conditions along these roads to mitigate potential problems with the addition of new trucks.

EXISTING PAVEMENT CONDITIONS

Our interpretation of the existing pavement condition is based upon a total of nine (9) pavement core samples collected along the alignments at the approximate locations shown on the Boring Location Maps (Figure No. 2) in Appendix "A", while the remaining is based on visual observations of the road surface made during the boring program. Refer to Appendix "B" for a pavement core summary and photographs for each pavement core obtained.

Based on visual observations, the pavement sections throughout the alignments consist of asphalt

6150 EAST 75TH STREET, INDIANAPOLIS, INDIANA 46250 PH. 317-576-8058 • FAX 317-576-1965 • WEB WWW.PATRIOTENG.COM INDIANA • BLOOMINGTON, EVANSVILLE, FORT WAYNE, INDIANAPOLIS, LAFAYETTE, TERRE HAUTE KENTUCKY • LOUISVILLE, OHIO • CINCINNATI, DAYTON, TENNESSEE • NASHVILLE pavement layers. The nine (9) pavement core samples collected varied in total thickness from approximately 5 to 17.5 inches. In boring B-4 and B-5, a layer of concrete was encountered beneath the asphalt surface. The concrete layer was about 6 to 7 inches thick. The crushed stone thicknesses below the pavement were approximately 2 to 8 inches thick. Crushed stone was not observed below the pavement section in boring B-4, B-5, and B-6.

A summary of the pavement thickness at each core location is shown below in Table No.1. Our interpretation of the existing pavement conditions is based upon visual observations made in our soil borings collected along the alignments at the approximate locations shown on the Boring Location Map (Figure No. 2) in Appendix "A".

Boring Location	Pavement ⁻	Thickness (in)	Crushed Stone Thickness (in)
Boring Location	Asphalt	Concrete	
B-1	14	-	2
B-2	12	-	2
B-3	13.5	-	3
B-4	6	7	-
B-5	3	6	-
B-6	17.5	-	-
B-7	10.5	-	8
B-8	10.5	-	8
В-9	5	-	4

 Table No. 1: Summary of Existing Pavement Thickness at Core Locations

Based on our experience, Patriot classified the relative conditions of the pavement cores obtained by visual observations of the wearing surface, apparent material layers soundness or quality, and visual observations of the bonding between layers. From our visual evaluations, nine (9) pavement cores appear to be in "fair condition". Note that the core samples showed minor problems such as voids within the surface and intermediate layers.

Additionally, the pavement surface along the roadway alignment was observed to be in fair condition. Minor edge cracking was noted as well as minor transverse and longitudinal cracking. Longitudinal and Transverse cracking is generally caused by issues with the pavement such as temperature changes, aging, and/or bonding during construction. The lack of edge support, such as a paved or stone shoulder was most likely the cause of the edge cracking observed.

SUBSURFACE CONDITIONS

Our interpretation of the subsurface conditions is based upon nine (9) soil borings drilled at the approximate locations shown on the Boring Location Map (Figure No. 2) in Appendix "A". Soil boring B-1 through B-9 were drilled along the existing roadway alignments.

The following discussion is general; for more specific information, please refer to the boring logs presented in Appendix "C". It should be noted that the dashed stratification lines shown on the soil boring logs indicate approximate transitions between soil types. In-situ stratification changes could occur gradually or at different depths. All depths discussed below refer to depths below the existing pavement surface. Our soil boring locations were not surveyed. However, existing ground surface elevations were provided based on the aerial maps.

The pavement is generally underlain by brown to gray, slightly moist to very moist, soft to hard silty and/or sandy clay. The silty and/or sandy clay layers typically extend to boring termination depths of 10 feet below the existing ground surface. The natural moisture content of these materials ranged from 7 to 27 percent (%). Standard Penetration Test N-values (blow counts) in this material varied from 3 to more than 50 blows per foot (bpf).

GROUNDWATER CONDITIONS

The term groundwater pertains to any water that percolates through the soil found on site. This includes any overland flow that permeates through a given depth of soil, perched water, and water that occurs below the "water table", a zone that remains saturated and water-bearing year-round.

Groundwater was not observed during drilling, nor upon completion of drilling activities. It should be recognized that fluctuations in the groundwater level should be expected over time due to variations in rainfall and other environmental or physical factors. The true static groundwater level can only be determined through observations made in cased holes over a long period of time, the installation of which was beyond the scope of this investigation.

EXPLORATIONAL PROCEDURES

A total of nine (9) soil borings were drilled, sampled, and tested at the project site between October 5, 2023, and October 6, 2023, at the approximate locations shown on the Boring Location Map (Figure No. 2) in Appendix "A". The depths that the soil borings were advanced to are shown on the Boring Logs in Appendix "A". All depths are given as feet below the existing ground surface.

The borings were advanced using 3¼ inch inside diameter hollow-stem augers. Samples were recovered in the undisturbed material below the bottom of the augers using the standard drive sample technique in accordance with ASTM D 1586-74. A 2 inch outside diameter by 13/8 inch inside diameter split-spoon sampler was driven a total of 18 inches with the number of blows of a 140-pound hammer falling 30 inches recorded for each 6 inches of penetration. The sum of blows for the final 12 inches of penetration is the Standard Penetration Test result commonly referred to

as the N-value (or blow-count). Split-spoon samples were recovered at 2.5 feet intervals, beginning at a depth of 1 foot below the existing surface grade, extending to a depth of 10 feet, and at 5 feet intervals thereafter to the termination of the boring.

Water levels were monitored at each borehole location during drilling and upon completion of the boring. The boreholes were backfilled with a mixture of auger cuttings and were patched prior to demobilization.

Upon completion of the boring program, samples retrieved during drilling were returned to Patriot's soil testing laboratory where they were visually examined and classified. A laboratory-generated log of each boring was prepared based upon the driller's field log, laboratory test results, and our visual examination. Test boring logs and a description of the classification system are included in Appendix "A" in this report. Indicated on each log are the primary strata encountered, the depth of each stratum change, the depth of each sample, the Standard Penetration Test results, groundwater conditions, and selected laboratory test data. The laboratory logs were prepared for each boring giving the appropriate sample data and the textural description and classification.

Representative samples recovered in the borings were selected for testing in the laboratory to evaluate their physical properties and engineering characteristics. Laboratory analysis includes natural moisture content determinations (ASTM D 2216), and an estimate of the cohesive soil strength was determined utilizing a hand penetrometer (qp). The results of laboratory tests are summarized in Section 3.2 "General Subsurface Conditions". Soil descriptions on the boring logs are in accordance with the Unified Soil Classification System (USCS).

Respectfully submitted, Patriot Engineering and Environmental, Inc.

Irfan Syed Geotechnical Engineer

Ben Lauletta, F

Project Engineer

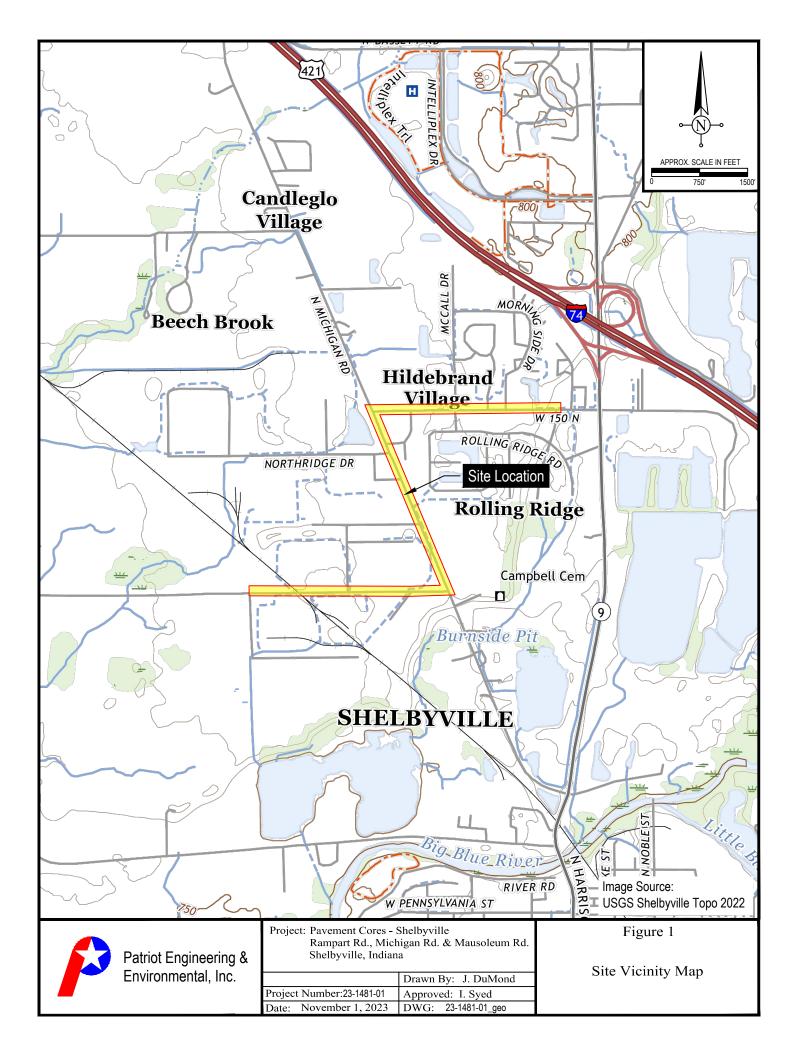


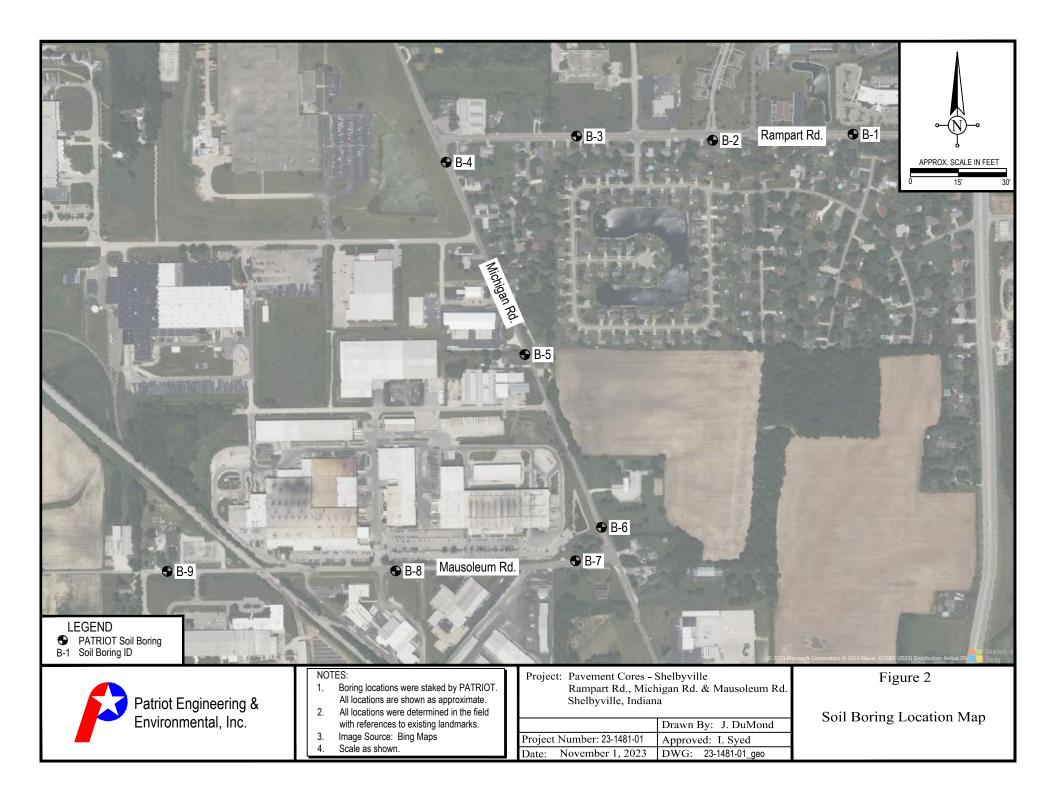
 Appendix A: Alignment Vicinity Map (Figure No. 1) Core/Boring Location Map (Figure No. 2)
 Appendix B: Pavement Core Summary & Photographs
 Appendix C: Boring Logs Boring Log Key Unified Soil Classification System (USCS)
 Appendix D: General Qualifications Standard Clause for Unanticipated Subsurface Conditions

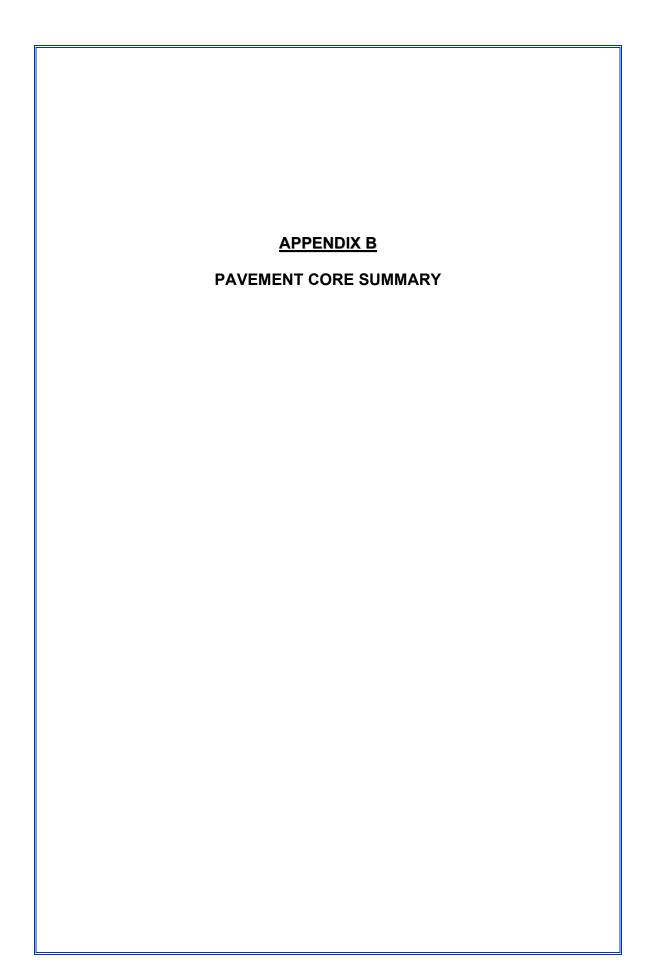
<u>APPENDIX A</u>

ALIGNMENT MAP (FIGURE NO. 1)

CORE/BORING LOCATION MAP (FIGURE NO. 2)







Pavement Cores – Shelbyville West Rampart Road Shelbyville, Indiana The City of Shelbyville Patriot Project No.: 23-1481-01G

Core No.	Date Cored	Core Dia.	Latitude	Longitude
B-1	10/05/2023	6"	39°32'51.12"N	85°46'42.06"W



Depth (in)	Pavement Type	Notes	Recovered Core Length (in)	In-hole Depth (in)	Recovery (%)
0 - 14	Asphalt	Intact	14	14	100
14 – 16	Crushed Stone	-	14	14	100

Pavement Cores – Shelbyville West Rampart Road Shelbyville, Indiana The City of Shelbyville Patriot Project No.: 23-1481-01G

Core No.	Date Cored	Core Dia.	Latitude	Longitude	
B-2	10/05/2023	6"	39°32'50.74"N	85°46'53.26"W	
			4 5 6 7 8 23-1481-016 B-2 12	and the second sec	

Depth (in)	Pavement Type	Notes	Recovered Core Length (in)	In-hole Depth (in)	Recovery (%)
0 – 12	Asphalt	Intact	10	10	100
12 – 14	Crushed Stone	-	12	12	100

Pavement Cores – Shelbyville West Rampart Road Shelbyville, Indiana The City of Shelbyville Patriot Project No.: 23-1481-01G

Core No.	Date Cored	Core Dia.	Latitude	Longitude
B-3	10/05/2023	6"	39°32'50.99"N	85°47'4.11"W



Depth (in)	Pavement Type	Notes	Recovered Core Length (in)	In-hole Depth (in)	Recovery (%)
0 – 13.5	Asphalt	Intact	12 5	12 5	100
13.5 – 16.5	Crushed Stone	-	13.5	13.5	100

Pavement Cores – Shelbyville North Michigan Road Shelbyville, Indiana The City of Shelbyville Patriot Project No.: 23-1481-01G

Core No.	Date Cored	Core Dia.	Latitude	Longitude
B-4	10/06/2023	6"	39°32'49.36"N	85°47'14.52"W



Depth (in)	Pavement Type	Notes	Recovered Core Length (in)	In-hole Depth (in)	Recovery (%)
0-6	Asphalt	Intact	10	10	100
6 -13	Concrete	Intact	13	13	100

Pavement Cores – Shelbyville North Michigan Road Shelbyville, Indiana The City of Shelbyville Patriot Project No.: 23-1481-01G

Core No.	Date Cored	Core Dia.	Latitude	Longitude
B-5	10/06/2023	6"	39°32'37.49"N	85°47'8.23"W



Depth (in)	Pavement Type	Notes	Recovered Core Length (in)	In-hole Depth (in)	Recovery (%)
0 – 3	Asphalt	Broken	0	0	100
3 -9	Concrete	Intact	9	9	100

Pavement Cores – Shelbyville North Michigan Road Shelbyville, Indiana The City of Shelbyville Patriot Project No.: 23-1481-01G

Core No.	Date Cored	Core Dia.	Latitude	Longitude
B-6	10/06/2023	6"	39°32'26.83"N	85°47'2.09"W



Depth (in)	Pavement Type	Notes	Recovered Core Length (in)	In-hole Depth (in)	Recovery (%)
0 – 17.5	Asphalt	Intact	17.5	17.5	100

Pavement Cores – Shelbyville West Mausoleum Road Shelbyville, Indiana The City of Shelbyville Patriot Project No.: 23-1481-01G

Core No.	Date Cored	Core Dia.	Latitude	Longitude
B-7	10/06/2023	6"	39°32'24.76"N	85°47'4.15"W



	Depth (in)	Pavement Type	Notes	Recovered Core Length (in)	In-hole Depth (in)	Recovery (%)
	0 – 10.5	Asphalt	Intact	10 5	10 5	100
ſ	10.5 – 18.5	Crushed Stone	-	10.5	10.5	100

Pavement Cores – Shelbyville West Mausoleum Road Shelbyville, Indiana The City of Shelbyville Patriot Project No.: 23-1481-01G

Core No.	Date Cored	Core Dia.	Latitude	Longitude
B-8	10/06/2023	6"	39°32'24.13"N	85°47'18.50"W



Depth (in)	Pavement Type	Notes	Recovered Core Length (in)	In-hole Depth (in)	Recovery (%)
0 – 10.5	Asphalt	Intact	10 5	10 5	100
10.5 – 18.5	Crushed Stone	-	10.5	10.5	100

Pavement Cores – Shelbyville West Mausoleum Road Shelbyville, Indiana The City of Shelbyville Patriot Project No.: 23-1481-01G

Core No.	Date Cored	Core Dia.	Latitude	Longitude
B-9	10/06/2023	6"	39°32'24.08"N	85°47'36.73"W



Depth (in)	Pavement Type	Notes	Recovered Core Length (in)	In-hole Depth (in)	Recovery (%)
0 – 5	Asphalt	Intact	F	F	100
5 – 9	Crushed Stone	-	5	5	100

APPENDIX C

BORING LOGS

BORING LOG KEY

UNIFIED SOIL CLASSIFICATION SYSTEM (USCS)

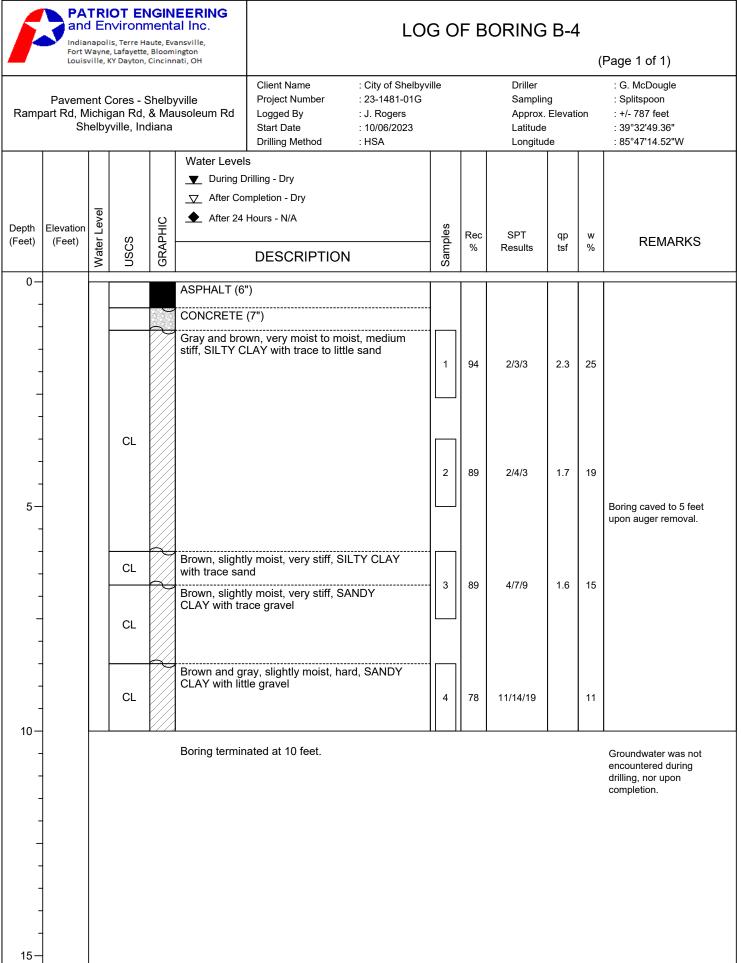
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- - - 5-			CL		Brown, moist sand	, stiff, SILTY CLAY v	vith trace	2	67	WOH/2/8	2.6	23	Boring caved to 4 feet upon auger removal. WOH - Weight of Hammer
-			CL		Brown, moist trace gravel a	, very stiff, SANDY (and trace shale	CLAY with	3	100	6/6/13		23	
-			CL		Brown, slightl SANDY CLA	y moist, medium stii Y with trace gravel	ff to stiff,	4	67	WOH/3/5	1.3	15	
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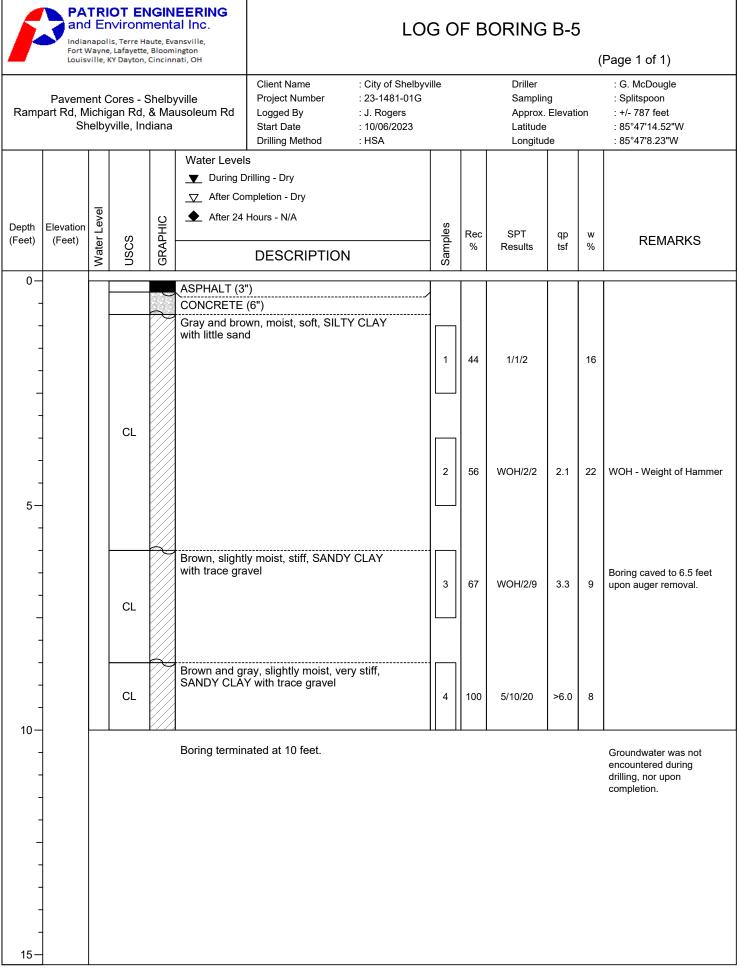
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ASPHALT (12")														
		CL		I ∖		AY with little	1	83	3/2/2		27			
		CL		Brown, slight SANDY CLA	ly moist, very stiff to Y with trace gravel	hard,	2	78	10/14/14	>6.0	7	Boring caved to 5.5 feet		
		CL		Gray and bro with trace sar	wn, moist, hard, SIL nd and little gravel	TY CLAY	3	44	9/18/29		22	upon auger removal.		
		CL		Brown, slight with trace gra	ly moist, hard, SANE avel	Y CLAY	4	100	11/21/25	>6.0	7			
			<u> </u>	Boring termin	ated at 10 feet.		111	11		<u> </u>		Groundwater was not encountered during drilling, nor upon completion.		
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				CRUSHED S Grav. moist. I	TONE (3") medium stiff, SILTY	CLAY with crete	1	44	2/3/3		22		
		CL		SILTY CLAY Brown, slightl	with trace sand ly moist, medium stif		2	44	3/3/5	4.2	15		
		CL		Brown, slightl	ly moist, very stiff to	hard, Iravel	3	100	3/10/15	>6.0	12	Boring caved to 6 feet upon auger removal.	
		CL					4	100	14/27/50-5"	>6.0	7		
				Boring termin	ated at 9.9 feet.							Groundwater was not encountered during drilling, nor upon completion.	
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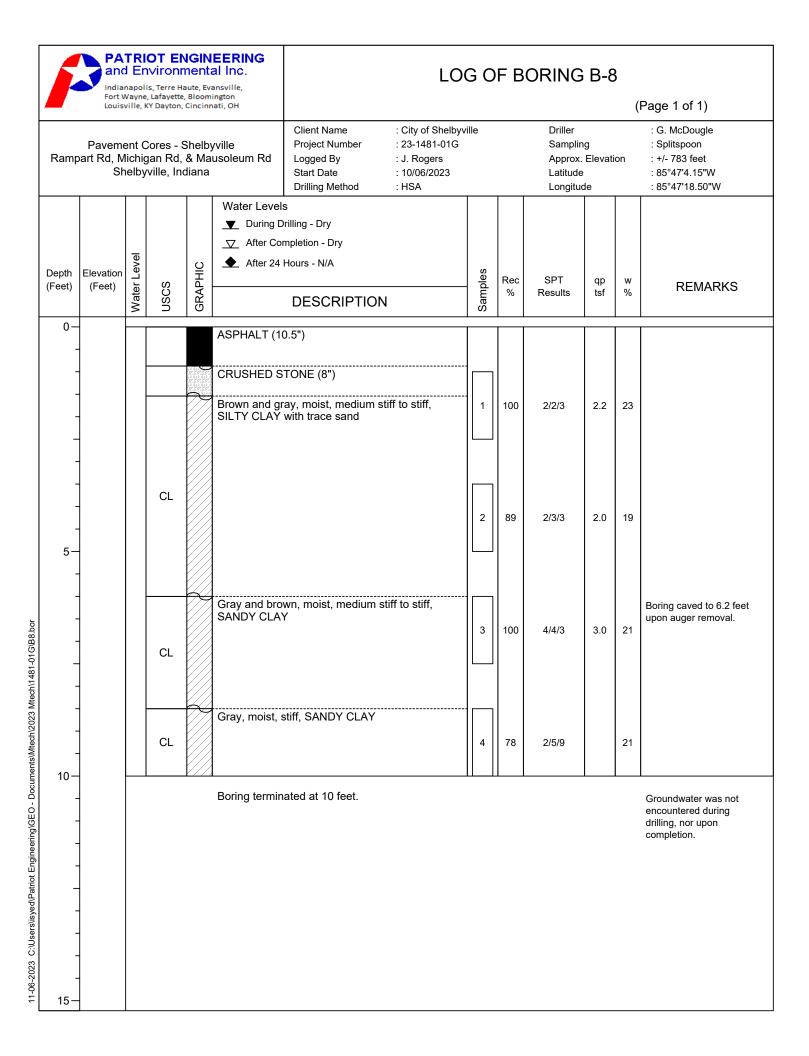


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Depth Feet)	Elevation (Feet)	Water Level	USCS	GRAPHIC	Water Level During E After Co After 24)rilling - Dry mpletion - Dry	N	Samples	Rec %	SPT Results	qp tsf	w %	REMARKS
-0	-				ASPHALT (1	7.5")							
-	-	-	CL		Brown, slight CLAY with tra	ly moist to moist, so ace gravel	ft, SANDY	1	56	1/1/2		15	
- - 5-	-	-	CL		Brown, moist CLAY with tra	, medium stiff to stif ace gravel	f, SANDY	2	78	2/2/4	2.0	18	Boring caved to 4.9 fee upon auger removal.
- - -	-	-	CL		Brown, slight with trace gra	ly moist, stiff, SAND avel and trace brick	Y CLAY	3	100	5/5/10	1.8	9	
-	-	-	CL		Brown, slight with trace gra	ly moist, hard, SANI avel	DY CLAY	4	89	15/23/30	>6.0	7	
10- - - -		<u> </u>		<u> </u>	Boring termir	nated at 10 feet.			<u> </u>		<u> </u>	L	Groundwater was not encountered during drilling, nor upon completion.
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	Fort W	/ayne	is, Terre Ha , Lafayette (Y Dayton,	Bloom	ington							((Page 1 of 1)	
Ramp		ichig		& Ma	/ville usoleum Rd	Client Name : City of Shelbyvi Project Number : 23-1481-01G Logged By : J. Rogers Start Date : 10/06/2023 Drilling Method : HSA			rille Driller Sampling Approx. Elevatio Latitude Longitude				: G. McDougle : Splitspoon n : +/- 785 feet : 39°32'24.76"N : 85°47'4.15"W	
Depth (Feet)	Elevation (Feet)	Water Level	USCS	GRAPHIC	Water Levels ▼ During D ▼ After Con ◆ After 24	rilling - Dry mpletion - Dry	1	Samples	Rec %	SPT Results	qp tsf	w %	REMARKS	
0-	ASPHALT (10.5")													
-			CL		CRUSHED S Brown and gr stiff, SANDY	TONE (8") ay, slightly moist, mo CLAY with little grav	edium stiff to el		89	2/3/3	2.8	10		
- - 5			CL		Brown, slightl SANDY CLA	y moist, medium stif Y with trace gravel	f to stiff,	2	67	1/3/3	2.2	10	Boring caved to 5.8 feet	
-			CL		Brown, slightl with trace gra	y moist, hard, SANE ivel	Y CLAY	3	100	6/15/23	>6.0	8	upon auger removal.	
-			CL		Brown and gr hard, SANDY	ay, slightly moist, ve ´CLAY with trace gra	ry stiff to avel	4	89	9/18/9	>6.0	7		
10 — - - - - - - - -					Boring termin	ated at 10 feet.			. 1				Groundwater was not encountered during drilling, nor upon completion.	

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and Environmental Inc. Indianapolis, Terre Haute, Evansville, Fort Wayne, Lafayette, Bloomington Louisville, KY Dayton, Cincinnati, OH					ington	LOG OF BORING B-9 (Page 1 of 1)							
Pavement Cores - Shelbyville Rampart Rd, Michigan Rd, & Mausoleum Rd Shelbyville, Indiana						Client Name: City of ShelbyvilleProject Number: 23-1481-01GLogged By: J. RogersStart Date: 10/06/2023Drilling Method: HSA				Driller Samplir Approx Latitude Longitu	. Elevati e	on	: G. McDougle : Splitspoon : +/- 778 feet : 39°32'24.08"N : 85°47'36.73"W
Depth	Elevation	Level		HIC	Water Level: During D After Con After 24	Drilling - Dry ompletion - Dry			Rec %	SPT Results	qp	w %	REMARKS
Feet)	(Feet)	Water Level	nscs	GRAPHIC	DESCRIPTION			Samples			tsf		
0— - -					ASPHALT (5 CRUSHED S Brown and gr CLAY with litt	-	SILTY						
-			CL					1	56	1/1/2		26	
- - 5			CL		Brown and gr stiff, SANDY	ay, slightly moist, mo CLAY with some gra	edium stiff to vel	2	78	2/3/4	2.5	11	
-			CL		Brown, slightl SANDY CLA interbedded s	ly moist, stiff to very Y with trace gravel a sand seams	stiff, nd	3	100	2/4/9	3.8	9	Boring caved to 7.2 feet upon auger removal.
-			CL		Brown, slightl with trace gra	ly moist, hard, SAND ivel	Y CLAY	4	100	6/15/23	>6.0	8	
10 — - - - - - -				<u>r</u> / / /	Boring termin	ated at 10 feet.			·			1	Groundwater was not encountered during drilling, nor upon completion.

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BORING LOG KEY

UNIFIED SOIL CLASSIFICATION SYSTEM FIELD CLASSIFICATION SYSTEM FOR SOIL EXPLORATION

NON COHESIVE SOILS

(Silt, Sand, Gravel and Combinations)

	Density		Grain Size Terminology							
Very Loos Loose	e -4 blows/ft. or les -5 to 10 blows/ft.	s <u>Soil</u>	Fraction	Particl	<u>e Size</u>	US Standard Sieve Size				
Medium D		. Boulde	rs	Larger thar	ו 12"	Larger than 12"				
Dense	-31 to 50 blows/ft		-	3" to12"		3" to 12"				
Very Dens			Coarse	³ ⁄ ₄ " to 3"		³ ⁄ ₄ " to 3"				
		0.0	Small	4.76mm to	3/4"	#4 to ¾"				
		Sand:	Coarse	2.00mm to		#10 to #4				
			Medium	0.42mm to		#40 to #10				
			Fine	0.074mm t		#200 to #40				
		Silt			o 0.074 mm	Smaller than #200				
		Clay			an 0.005mm	Smaller than #200				
		ELATIVE PRC		FOR SOILS	5					
		Descriptive Terr	<u>n</u>	Percent						
		Trace		1 - 10						
		Little		11 - 20						
		Some		21 - 35						
		And		36 - 50						
			HESIVE SO	-						
			(Clay, Silt and Combinations) Unconfined Compressive			fication (Approx.)				
	Consistency		gth (tons/sq.		SPT Blows/ft.					
-										
	Very Soft	-	ss than 0.25		0 - 2					
	Soft	-	.25 – < 0.5		3 - 4 5 - 8 9 -15					
	Medium Stiff		0.5 - < 1.0							
	Stiff		1.0 - < 2.0							
	Very Stiff	:	2.0 - < 4.0			16 - 30				
	Hard		Over 4.0			> 30				

<u>Classification</u> on logs are made by visual inspection.

Standard Penetration Test - Driving a 2.0" O.D., $1^{3/8}$ " I.D., sampler a distance of 1.0 foot into undisturbed soil with a 140 pound hammer free falling a distance of 30.0 inches. It is customary for **Patriot** to drive the spoon 6.0 inches to seat into undisturbed soil, then perform the test. The number of hammer blows for seating the spoon and making the tests are recorded for each 6.0 inches of penetration on the drill log (Example - 6/8/9). The standard penetration test results can be obtained by adding the last two figures (i.e. 8 + 9 = 17 blows/ft.).

<u>Strata Changes</u> - In the column "Soil Descriptions" on the drill log the horizontal lines represent strata changes. A solid line (_____) represents an actually observed change, a dashed line (- - - - -) represents an estimated change.

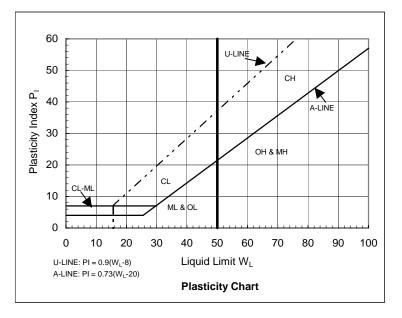
<u>Groundwater</u> observations were made at the times indicated. Porosity of soil strata, weather conditions, site topography, etc., may cause changes in the water levels indicated on the logs.

Groundwater symbols: ▼-observed groundwater elevation, encountered during drilling; ∇-observed groundwater elevation upon completion of boring.



Unified Soil Classification System

	Major Divisio	ns	Group	o Symbol	Typical Names	Classification Criteria for Coarse-Grained Soils					
	arse No. 4	Clean gravels (little or no fines)	GW		Well-graded gravels, gravel-sand mixtures, little or no fines	C _U ≥4 1 <u><</u> C _C ≤ 3	$\begin{array}{c} C_{U} \ge 4 \\ I \le C_{C} \le 3 \end{array} \qquad C_{U} = \begin{array}{c} D \\ -D \\ D \end{array}$		$C_{C} = \frac{D_{30}^{2}}{D_{10}D_{60}}$		
o. 200)	Gravels an half of co larger than eve size)	Clean (little fin	GP		Poorly graded gravels, gravel-sand mixtures, little or no fines		Not meeting all gradation requirements f GW ($C_U < 4 \text{ or } 1 > C_C > 3$)				
s er than N	Gravels (more than half of coarse fraction is larger than No. 4 sieve size)	Gravels with fines (appreciable amount of fines)	GM	<u>d</u> u	Silty gravels, gravel-sand-silt mixtures	Atterberg limits A line or P _I -			ove A line with $4 < P_1 < 7$		
Coarse-grained soils (more than half of material is larger than No. 200)	(mo fracti	Gravels with fines (appreciable amount of fines)	GC		Clayey gravels, gravel-sand-clay mixtures	Atterberg limits above requiring us			oorderline cases iring use of dual symbols		
	arse No. 4	Clean sands (little or no fines)	SW		Well-graded sands, gravelly sands, little or no fines	$\begin{array}{c} C_{U} \ge 6 \\ 1 \le C_{C} \le 3 \end{array} \qquad C_{U} = \begin{array}{c} D_{60} \\ D_{10} \end{array}$			$C_{C} = \frac{(D_{30})^{2}}{D_{10} D_{60}}$		
C than half	Sands han half of co s smaller than sieve size)	Clean (little fin	SP		Poorly graded sands, gravelly sands, little or no fines		Not meeting all gradation requirements f SW ($C_U < 6$ or $1 > C_c > 3$)				
(more t	Sands (more than half of coarse fraction is smaller than No. 4 sieve size)	s with es ciable nt of ss)	SM $\frac{d}{u}$ SC		Silty sands, sand-silt mixtures		Atterberg limits below A line or $P_1 < 4$ zone with $4 \le P_1 \le 7$				
	(mc fractic	Sands with fines (appreciable amount of fines)			Clayey sands, sand-clay mixtures	Atterberg limits above A line with P ₁ > 7 A line with P ₁ > 7			iring use of dual		
500)	g	ML		Inorganic silts and very fine sands, rock flour, silty or clayey fine sands, or clayey silts with slight plasticity	 Determine percentages of sand and gravel from grain size curve. Depending on percentages of fines (fraction smalle 						
than No. 2	Silt and clays		CL	Inorganic clays of low to medium plasticity, gravelly clays, sandy clays, silty clays, lean clays	than 200 sieve size), coarse-grained soils are classified as follows: Less than 5% - GW, GP, SW, SP More than 12% - GM, GC, SM, SC						
Fine-grained soils (more than half of material is smaller than No. 200)	05	OL		Organic silts and organic silty clays of low plasticity	5-12% - Borderline cases requiring dual symbols						
	lays		MH	Inorganic silts, micaceous or diatomaceous fine sandy or silty soils, elastic silts							
	Sitts and clays	СН		Inorganic clays or high plasticity, fat clays							
	Silts	ОН		Organic clays of medium to high plasticity, organic silts							
(more	Highly	РТ		Peat and other highly organic soils							



APPENDIX D

GENERAL QUALIFICATIONS

STANDARD CLAUSE FOR UNANTICIPATED SUBSURFACE CONDITIONS

GENERAL QUALIFICATIONS

of Patriot Engineering's Geotechnical Engineering Investigation

This report has been prepared at the request of our client for his use on this project. Our professional services have been performed, findings obtained, and recommendations prepared in accordance with generally accepted geotechnical engineering principles and practices. This warranty is in lieu of all other warranties either expressed or implied.

The scope of our services did not include any environmental assessment or investigation for the presence or absence of wetlands, hazardous or toxic materials in the soil, groundwater, or surface water within or beyond the site studied. Any statements in this report or on the test borings logs regarding vegetation types, odors or staining of soils, or other unusual conditions observed are strictly for the information of our client and the owner.

This report may not contain sufficient information for purposes of other parties or other uses. This company is not responsible for the independent conclusions, opinions or recommendations made by others based on the field and laboratory data presented in this report. Should there be any significant differences in structural arrangement, loading or location of the structure, our analysis should be reviewed.

The recommendations provided herein were developed from the information obtained in the test borings, which depict subsurface conditions only at specific locations. The analysis, conclusions, and recommendations contained in our report are based on site conditions as they existed at the time of our exploration. Subsurface conditions at other locations may differ from those occurring at the specific drill sites. The nature and extent of variations between borings may not become evident until the time of construction. If, after performing on-site observations during construction and noting the characteristics of any variation, substantially different subsurface conditions from those encountered during our explorations are observed or appear to be present beneath excavations, we must be advised promptly so that we can review these conditions and reconsider our recommendations where necessary.

If there is a substantial lapse of time between the submission of our report and the start of work at the site, or if conditions have changed due to natural causes or construction operations at or adjacent to the site, we urge that our report be reviewed to determine the applicability of the conclusions and recommendations considering the changed conditions and time lapse.

We urge that Patriot be retained to review those portions of the plans and specifications that pertain to earthwork and foundations to determine whether they are consistent with our recommendations. In addition, we are available to observe construction, particularly the compaction of structural backfill and preparation of the foundations, and such other field observations as may be necessary.

In order to fairly consider changed or unexpected conditions that might arise during construction, we recommend the following verbiage (Standard Clause for Unanticipated Subsurface Conditions) be included in the project contract.

STANDARD CLAUSE FOR UNANTICIPATED SUBSURFACE CONDITIONS

"The owner has had a subsurface exploration performed by a soils consultant, the results of which are contained in the consultant's report. The consultant's report presents his conclusions on the subsurface conditions based on his interpretation of the data obtained in the exploration. The contractor acknowledges that he has reviewed the consultant's report and any addenda thereto, and that his bid for earthwork operations is based on the subsurface conditions as described in that report. It is recognized that a subsurface exploration may not disclose all conditions as they actually exist and further, conditions may change, particularly groundwater conditions, between the time of a subsurface exploration and the time of earthwork operations. In recognition of these facts, this clause is entered in the contract to provide a means of equitable additional compensation for the contractor if adverse unanticipated conditions are encountered and to provide a means of rebate to the owner if the conditions are more favorable than anticipated.

At any time during construction operations that the contractor encounters conditions that are different than those anticipated by the soils consultant's report, he shall immediately (within 24 hours) bring this fact to the owner's attention. If the owner's representative on the construction site observes subsurface conditions which are different than those anticipated by the consultant's report, he shall immediately (within 24 hours) bring this fact to the consultant's report, he shall immediately (within 24 hours) bring this fact to the consultant's report, he shall immediately (within 24 hours) bring this fact to the contractor's attention. Once a fact of unanticipated conditions has been brought to the attention of either the owner or the contractor, and the consultant has concurred, immediate negotiations will be undertaken between the owner and the contractor to arrive at a change in contract price for additional work or reduction in work because of the unanticipated conditions. The contract agrees that the following unit prices would apply for additional or reduced work under the contract. For changed conditions for which unit prices are not provided, the additional work shall be paid for on a time and materials basis."

Another example of a changed conditions clause can be found in paper No. 4035 by Robert F. Borg, published in <u>ASCE Construction Division Journal</u>, No. CO2, September 1964, page 37.